

LIMITED-APERTURE TRUE-AMPLITUDE KIRCHHOFF DEPTH MIGRATION—A NEW CONCEPT AND PRELIMINARY RESULTS

I. Veile and J. Mann

email: *Ines.Veile@gpi.uka.de*

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ABSTRACT

In Kirchhoff migration, the proper choice of the aperture is essential: the optimum aperture is the limited aperture defined by the projected Fresnel zone. This is the smallest aperture providing interpretable amplitudes along with the highest possible S/N ratio and the minimum number of required summations. In addition, limited-aperture migration naturally prevents operator aliasing. The common-reflection-surface stack provides kinematic wavefield attributes which allow to estimate the optimum aperture size for zero-offset and its dislocation with varying offset. The aperture is centered around the stationary point, but this point has to be associated with the corresponding point in the migrated domain in an additional process. Kirchhoff migration itself implicitly connects the stationary point and the image point in depth by collecting the energy in the vicinity of the former and assigning it to the latter. In principle, any smoothly varying property can be migrated “on top” of the seismic data themselves by applying multiple weighted diffraction stacks. The most generic property to be migrated in this way is the source/receiver midpoint which yields the stationary point mapped to the image location in depth. We investigate the validity and accuracy of this approach for simple synthetic data and apply it to a real land data set. A simple extension is introduced to solve most of the numerical problems inherent to this approach.

INTRODUCTION

In Kirchhoff migration the migrated time or depth image is generated by a summation along the forward-calculated diffraction traveltime surfaces (or Huygens surfaces) in the unmigrated domain. From a theoretical point of view, this summation has to be performed within an infinite aperture. Practically, the aperture is limited by the acquisition geometry, the recording time, and the computational costs. Schleicher et al. (1997) showed that the optimum limited aperture is the minimum aperture defined by the first projected Fresnel zone. Together with appropriate tapering within the adjacent second projected Fresnel zone, this yields interpretable amplitudes along the reflector images and the minimum number of required summations. As the summation is only carried out where the reflection event and the migration operator are virtually tangent to each other, this approach automatically prevents operator aliasing and minimizes the unwanted contributions from other events and background noise usually gathered along the remaining, non-tangent part of the migration operator.

The common-reflection-surface (CRS) stack method (see, e. g., Mann et al., 1999; Jäger et al., 2001) provides kinematic wavefield attributes which allow to estimate various properties relevant for Kirchhoff migration: the geometrical spreading factor required for true-amplitude migration, as well as the projected Fresnel zone for zero-offset and the common-reflection-point (CRP) trajectory describing the dislocation of the stationary point with varying offset. The latter are well suited to estimate the size of the limited aperture and its dislocation with offset. However, the absolute location of the aperture, the stationary point, has to

be associated with the corresponding depth point in the migrated domain to actually perform Kirchhoff migration.

One strategy to determine the stationary point associated with a given image location in the migrated domain is to directly evaluate the tangency criterion between the migration operator and the reflection event. For the latter, the dip for offset zero is available from the CRS wavefield attributes such that the problem reduces to the determination of the migration operator dip for zero offset. In the next step, the stationary point found for offset zero is extrapolated along the CRP trajectory to finite offsets.

Spinner and Mann (2005, 2006) used this concept in true-amplitude limited-aperture time migration. Based on a straight ray approximation, the required operator dip can be directly calculated from the analytic migration operator in this case. In contrast, for depth migration the migration operator will, in general, be of complex shape and an analytic approximation is no longer appropriate. To follow the tangency-based strategy here, Jäger (2005a,b) proposed to numerically calculate the migration operator dip by means of a finite-difference scheme from the Green's function tables (GFTs) on the fly during migration. Obviously, this approach is sensitive to the smoothness of the GFTs and, thus, to the smoothness of the underlying macro-velocity model.

In this paper we want to investigate whether Kirchhoff migration itself is also suited to determine the stationary points in a stable and reliable way. Kirchhoff migration itself is far less sensitive to the smoothness of the GFTs than an operator dip calculated with the finite difference scheme. Kirchhoff migration is a linear process. In addition, Kirchhoff migration only generates a significant output amplitude if a stationary point exists in the unmigrated domain. This implies that under certain conditions, a *local* scaling or weighting can be migrated “on top” of the seismic data. The most generic property to be migrated in this way is the source/receiver midpoint which directly yields the stationary point as a function of the image location.

In the following, we investigate the validity and accuracy of this so-called double-diffraction stack approach for the determination of the stationary point with simple synthetic data and apply the scheme to a real land data set. Using the trace envelopes we can overcome most of the numerical problems typical for the double diffraction stack approach.

DOUBLE DIFFRACTION STACK

Tygel et al. (1993) established the so-called double diffraction stack. Originally, it was intended to economize true-amplitude migration. We will show that this method is also able to support the CRS-based limited-aperture Kirchhoff migration.

Let us briefly review the basics of the diffraction stack method. For the sake of simplicity considering a planar measurement surface, each source location and each receiver location is defined by the parameter vector $\vec{\xi} = (\xi_1, \xi_2)$ that is confined to the aperture A . Using a given macro-velocity model, the traveltimes from each source or receiver to all points in the target zone are computed. This allows to calculate the diffraction traveltime t_D for any source/receiver combination associated with a given $\vec{\xi}$ with respect to a given depth point M , i. e., the Huygens surface $t_D(\vec{\xi}, M)$. The actual diffraction stack is then based on a summation along this Huygens surface in the prestack data. The output

$$V_j(M) = -\frac{1}{2\pi} \iint_A d\xi_1 d\xi_2 w_j(\vec{\xi}, M) \times \dot{U}(\vec{\xi}, t) \Big|_{t=t_D(\vec{\xi}, M)}$$

yields only a significant value if the point M lies close to a reflector. The time derivative (or half derivative in 2.5D) of U is required to restore the original wavelet. The weight w_j can be chosen such that it compensates for geometrical spreading in a true-amplitude migration. For a purely kinematic migration $w_j = 1$.

In principle, we can use any kind of weighting w_j during migration, provided that the weight function is smoothly varying with $\vec{\xi}$. According to the method of stationary phase (Bleistein, 1984), we will only receive contributions from the vicinity of the stationary point, of course, requiring appropriate tapering. Due to the linearity of the process, the migration result will be locally weighted with the weight w_j applied at the stationary point.

This leads to the general idea of the double diffraction stack, i. e., to perform Kirchhoff migration twice with two different weights, once with unit weight and once with a weight that carries the desired

superimposed information. The ratio of the two migration results recovers the superimposed information at the migrated location. Since we try to find a reliable method to determine the stationary point which is characterized by the trace location it stands to reason that the trace location is used as the second migration weight. Accordingly, the ratio of the migration results directly represents the locations of the stationary points.

In practice, we have to consider that the double diffraction stack results are only valid and reliable along reflector images. The structure of the data accounts for the correct positioning of the result. One consequence is that it is completely impossible to migrate the weight function without the underlying seismic data. In addition, we need criteria to decide where the stationary point is well defined. Numerically, we can expect that the approach is impeded by unstable results at locations with small amplitudes in both diffraction stack results, e. g., at zero crossings of the wavelet.

SYNTHETIC DATA EXAMPLE

In this section we investigate a very simple synthetic data set to get some idea of the area in which the stationary point is valid and of its sensitivity with respect to the overall noise level. The model consists of two horizontal reflectors at depths of 1000 m and 2500 m with the same reflectivity embedded in a homogeneous background model with a velocity of 2000 m/s. This model definition has several advantages in this context:

- Migration is possible using analytical operators. Thus, potential errors in the macro-velocity model or in the corresponding GFTs cannot occur.
- The flat reflectors allow to use small migration apertures to exclude the risk of operator aliasing.
- Amplitudes can be extracted from the migration results along a well-defined constant depth level. Explicit picking and tracking of event is not required.
- Due to its 1D nature, the stationary point should just represent the image location where it is defined. In other words, the relative displacement of this locations is a direct indicator of the obtained error.

For this model, we simulated a ZO data set with the primary reflection responses consisting of 351 traces with a sampling interval of 4 ms and a shot spacing of 20 m. The signal is a Ricker wavelet with a peak frequency of 40 Hz. Note that despite the identical reflectivity of the reflectors, the second reflection event appears far weaker due to the larger geometrical spreading. Colored noise of various different levels has been superimposed to the data.

Each seismic trace has been multiplied with its shot position to obtain the weighted input for the double diffraction stack. Poststack Kirchhoff migration was applied to the original and the weighted data, with a target zone of 5000 m width and 3000 m depth at sampling rates of 20 m and 5 m, respectively. The aperture linearly varies between 100 m and 500 m with increasing target depth. Finally, we computed the ratio of the two migration results to recover the stationary point. Figure 1 (top) shows the section with this ratio for a S/N ratio¹ of 40. At a first glance, the stationary point location seems to closely follow the lateral image location, even in the noisy areas in between the two reflector images! The latter phenomenon can be easily explained: the used aperture is symmetric with respect to the considered lateral image location. In the noisy areas, the migration effectively averages all trace locations within the aperture with random weighting factors. This average scatters around the unweighted average, i. e., the center of the aperture which coincides with the lateral image location.

Obviously, this way of displaying the results is of little use as the large variation of the weight function along the section completely obscures any local variations. For this 1D model, the actual stationary point along the reflector images should coincide with the lateral image location. Thus, a section of the relative lateral displacement between these two locations is far better suited to analyze the validity and accuracy of the results: Figure 1 (bottom) immediately reveals that the result in the noisy areas is as random as expected, whereas the result along the reflector images is close to the expected zero displacement.

For a systematic analysis of this displacement as a function of the S/N ratio and the position within the wavelet, we consider the average absolute displacement error along constant depth levels. For the

¹In this paper S/N ratio refers to the correspondent parameter of the Seismic Un*x utility `suaddnoise`.

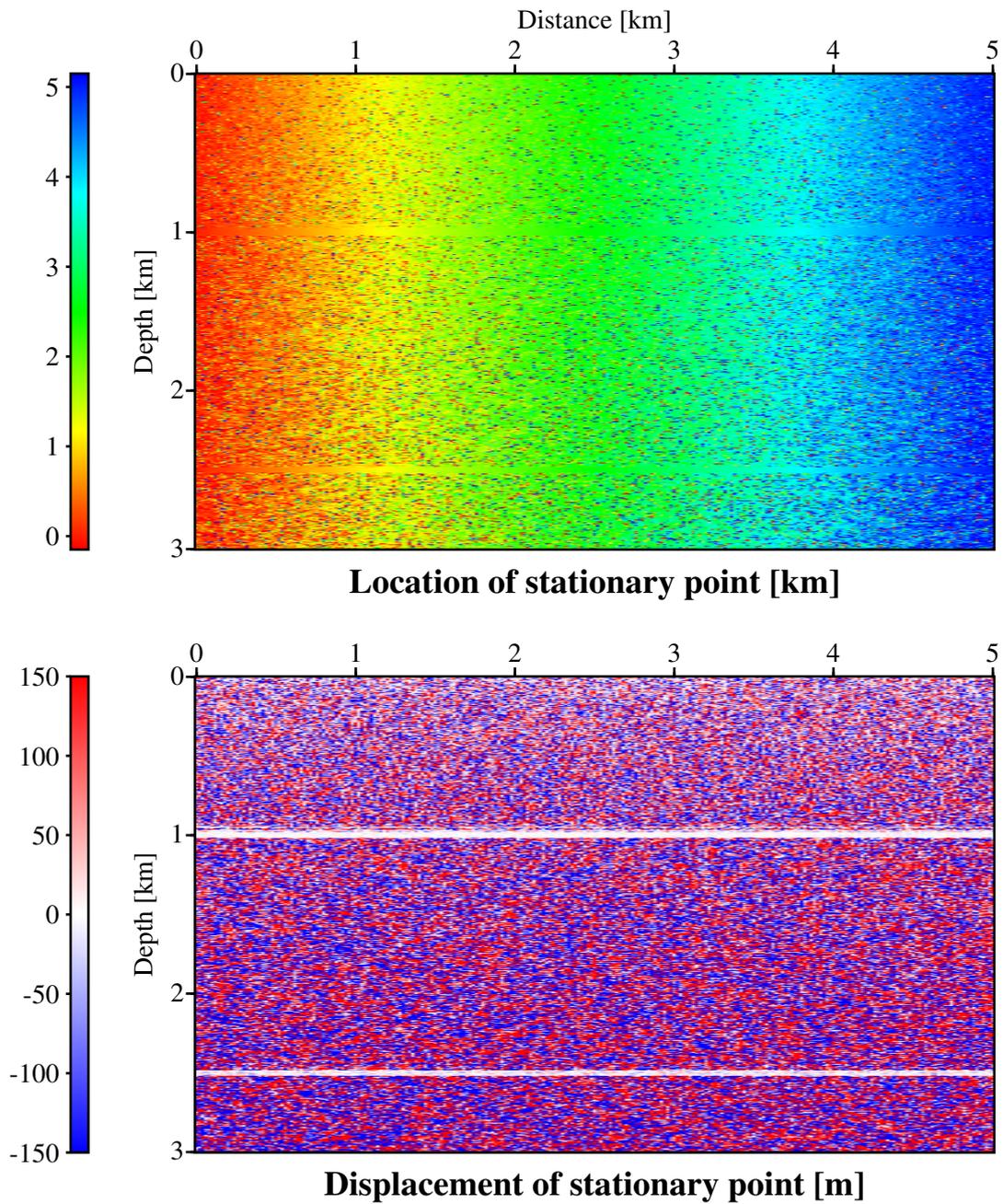


Figure 1: Synthetic data: top: location of the stationary point given by the ratio of the double diffraction stack results. Bottom: displacement of stationary point with respect to the lateral image position.

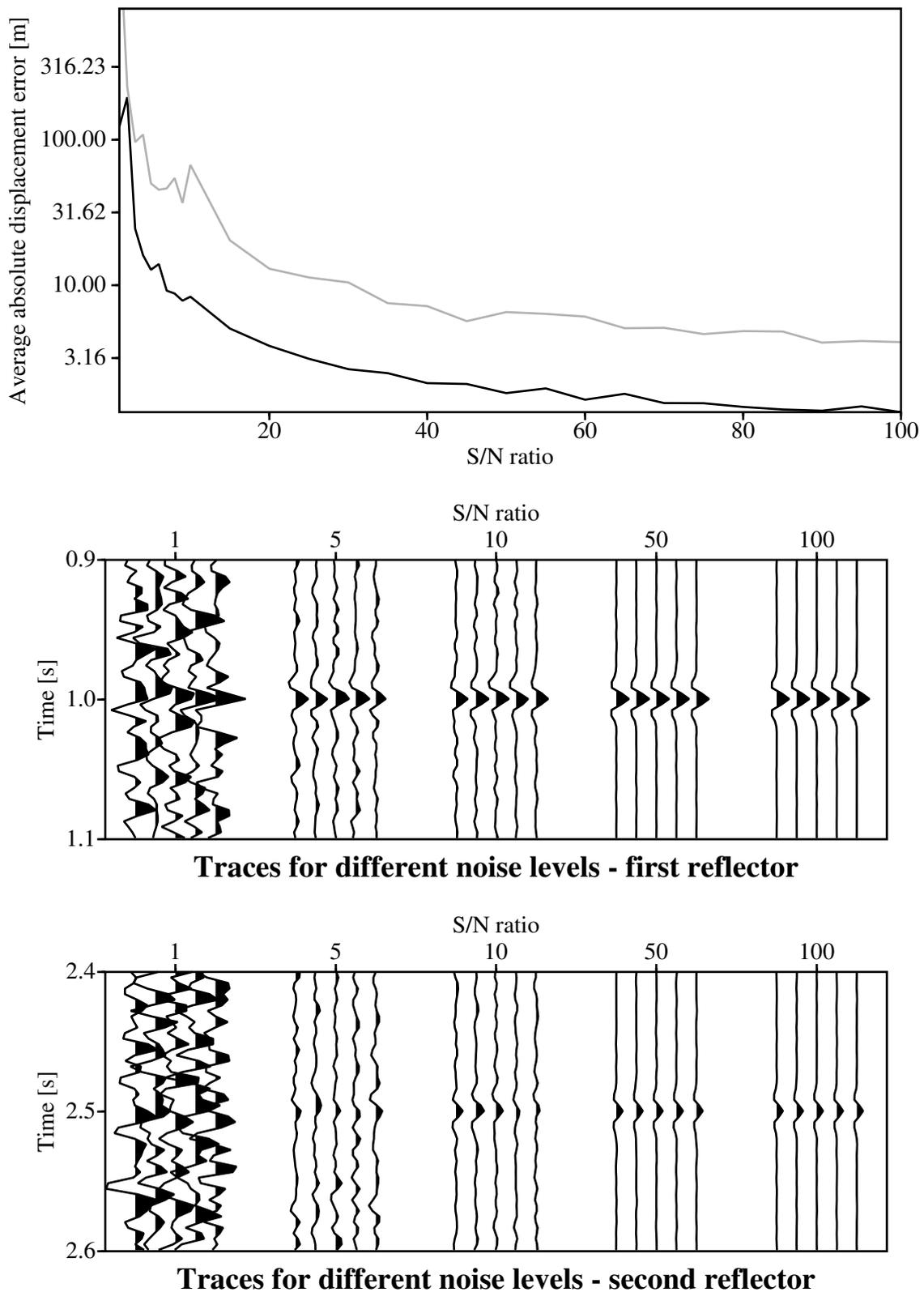


Figure 2: Synthetic data: top: semilogarithmic display of the average absolute displacement error for first (black) and second (gray) reflector. Representative traces for different noise levels for the first (middle) and second (lower) reflector.

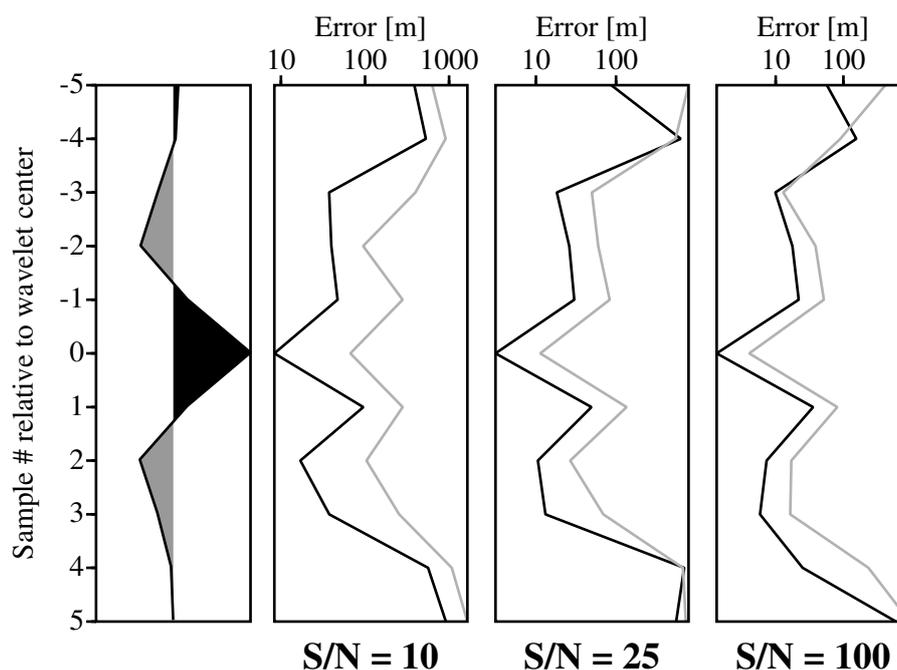


Figure 3: Synthetic data: left: migrated Ricker wavelet (without noise). Right: semilogarithmic representation of the average absolute displacement error along the wavelet for first (black) and second (gray) reflector for three different noise levels. Note the different horizontal scales. Depth sampling interval is 5 m.

center of the Ricker wavelet, the average absolute displacement error is displayed in Figure 2 (top) for various noise levels. The lower part of Figure 2 shows some representative traces for different noise levels. For reasonably high S/N ratios, the average error is far smaller than the size of the projected Fresnel² zone, which is ≈ 320 m for the first and ≈ 500 m for the second reflector. Considering the usually quite unrealistic properties of synthetic noise, we can expect an even higher accuracy for real data.

In the next step, we analyze the average absolute displacement error in a similar manner along the seismic wavelet. Figure 3 displays this error as a function of the distance to the center of the wavelet for three different noise levels together with the original, noise-free wavelet. We can clearly observe that the error varies significantly along the wavelet. Especially at zero crossings, the error strongly increases. This directly reflects the expected numerical problems occurring for small amplitudes in the both migrations results used to compute the stationary points. As the displacement errors quickly exceed any acceptable limit at such locations, we will address this problem in the real data example below.

REAL LAND DATA EXAMPLE

The 2D seismic land dataset discussed in the following was acquired by an energy resource company in a fixed-spread geometry. The seismic line has a total length of about 12 km. The utilized source signal was a linear upsweep from 12 to 100 Hz of 10 s duration. Shot and receiver spacing are both 50 m and the temporal sampling interval is 2 ms. Standard preprocessing was applied to the field data including the setup of the data geometry, trace editing, deconvolution, geometrical spreading correction, field static correction, and bandpass filtering. The underlying structure consists of nearly horizontal layers and some dipping layers due to dip faulting in some parts. An entire imaging sequence consisting of CRS stack, NIP wave tomography, and limited aperture poststack and prestack Kirchhoff migration for these data can be found in Hertweck et al. (2004). We used the same CRS-stacked section and the same GFTs for the application of the double diffraction stack. All migration parameters have been pertained to make the results comparable:

²Calculated for a monochromatic signal of 40 Hz.

the target grid is sampled with 20 m in lateral and 4 m in vertical direction. The symmetric aperture has an half-width varying from 60 m to 450 m from top to bottom.

As for the synthetic data, we weighted the input data, here the CRS stack result, with the shot location of each trace. Two independent migrations have been performed, one of the weighted and one of the unweighted input, respectively. Figure 4 shows the migration result for the unweighted input together with the ratio of the two migration results. Again, the direct display of the stationary point is quite pointless as it does not provide the required resolution. The same applies to similar double diffraction stack results as, e. g., presented by Chen (2004).

To obtain an interpretable result, we again calculated the relative displacement of the stationary point with respect to the lateral image location in depth. In contrast to our synthetic example where the exact displacement is zero, this displacement will, in general, not vanish for the real data. Figure 5 shows this displacement with an obvious correlation to the dip of the reflector images: we can directly observe the lateral component of the well-known up-dip movement during migration.

In Figure 6 we see some details of Figures 4 and 5. A coherence-based criterion has been applied to mask out samples not located on reflector images. We can clearly observe the same numerical problems as for the synthetic data: the stationary point gets unacceptably inaccurate at zero-crossings of the wavelet. In its original form, i.é., the ratio of the diffraction stack results, the accuracy of the stationary point is below reasonable limits and, thus, of no practical use. Unfortunately, other publications on double diffraction stack like Chen (2004) do not comment on this problem and its solution.

To overcome these numerical problems occurring at zero-crossings we have to get rid of the corresponding phase behavior of the wavelet. This can be achieved in a strikingly straightforward way if we calculate the envelope of the analytic signal for both diffraction stack results *before* computing their ratio. Naturally, the envelope is non-zero along the entire wavelet. Therefore, the numerical problems should completely disappear. Indeed, this can be readily seen in the lower parts of Figures 5 and 6: the displacement of the stationary point is now stable along the entire wavelet. The remaining variations are most likely due to migration noise and are well below the size of the projected first Fresnel zone.

CONCLUSIONS & OUTLOOK

We have revisited the double diffraction stack approach proposed by Tygel et al. (1993). In this paper, our intention is to use it as a simple and efficient method to calculate the relation between the stationary point in the unmigrated domain and the corresponding image point in the depth-migrated domain. In principle, this allows to correctly place the migration aperture in limited aperture migration and to extract the CRS wavefield attributes defined at the stationary point. These attributes provide information on the aperture size and its behavior with varying offset and, thus, all information required to perform limited-aperture migration (see, e. g., Jäger, 2005a; Spinner and Mann, 2005).

The direct calculation of the stationary point as ratio of the two diffraction stack results turned out to be unstable and unreliable especially at zero-crossings of the wavelet. With an extension of this approach we can completely overcome the occurring numerical problems and obtain stable results along the entire wavelet: we compute the envelopes of the analytic signals of the two diffraction stack results prior to calculating their ratio. The local amplitude properties of the signal are fully preserved, but the zero-crossings vanish. This approach is as simple as efficient and finally provides useful input for limited-aperture migration. Beyond that, all kinds of application of the double diffraction stack will benefit from this extension in a similar way.

The next step towards the actual application of these results in limited-aperture migration is the automatic extraction of the reliable stationary points from the double diffraction stack results. First experiments suggest that this can be easily achieved by adopting the CRS strategies to the migrated depth domain. This includes the determination of dip and curvature of the reflector images using the linear and hyperbolic ZO stacks (see, e. g. Mann, 2002) followed by the event-consistent smoothing approach proposed by Mann and Duvencck (2004) to remove the migration noise. As it is well known from its application in the time domain, the CRS method also provides a coherence section. Combined with a suitable coherence threshold to select the locations with reliable results, the determined stationary points can then be used as an alternative to their counterparts computed on-the-fly based on GFTs as proposed by Jäger (2005a).

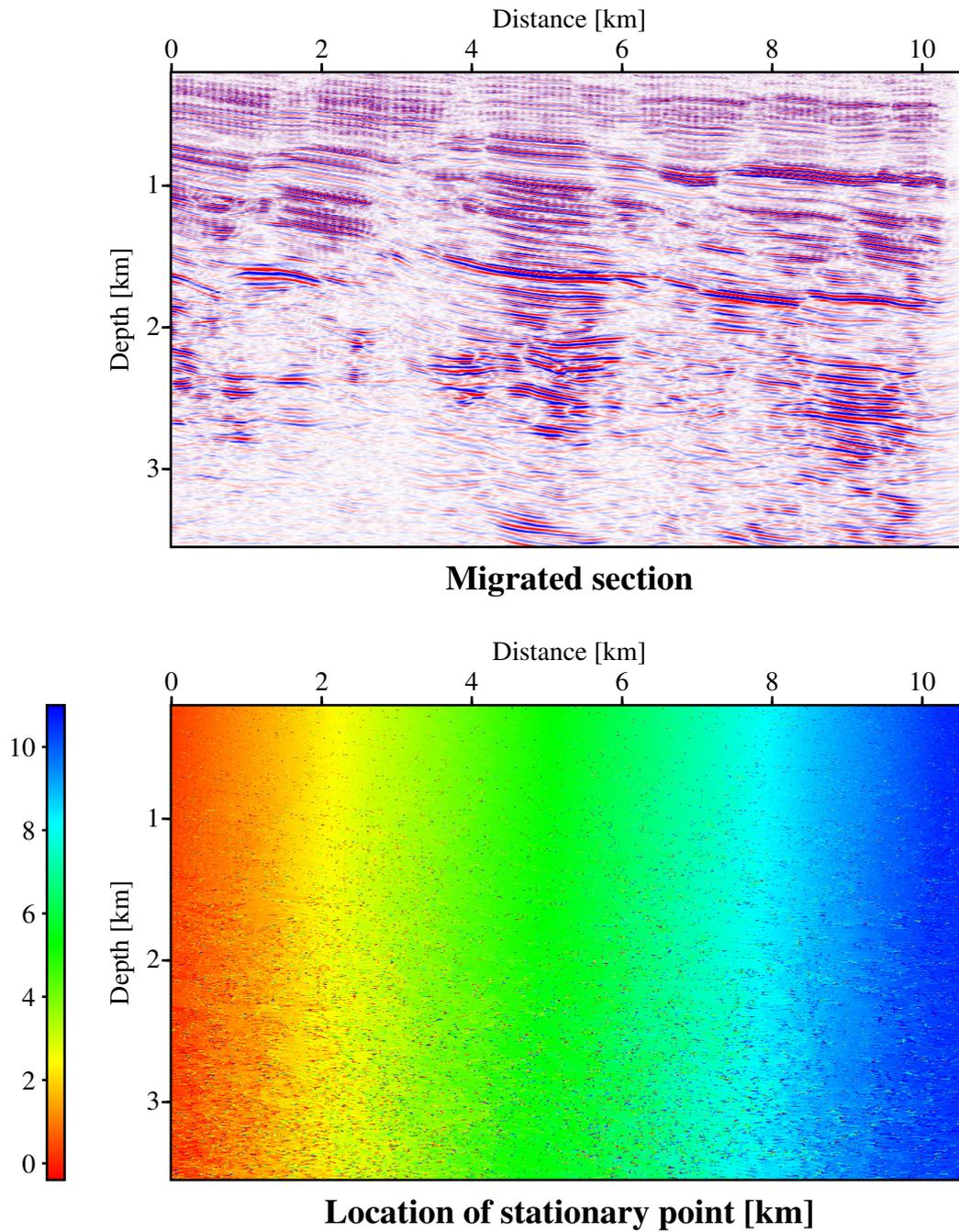


Figure 4: Real land data: top: unweighted poststack depth migration result. Bottom: location of the stationary point given by the ratio of the double diffraction stack results.

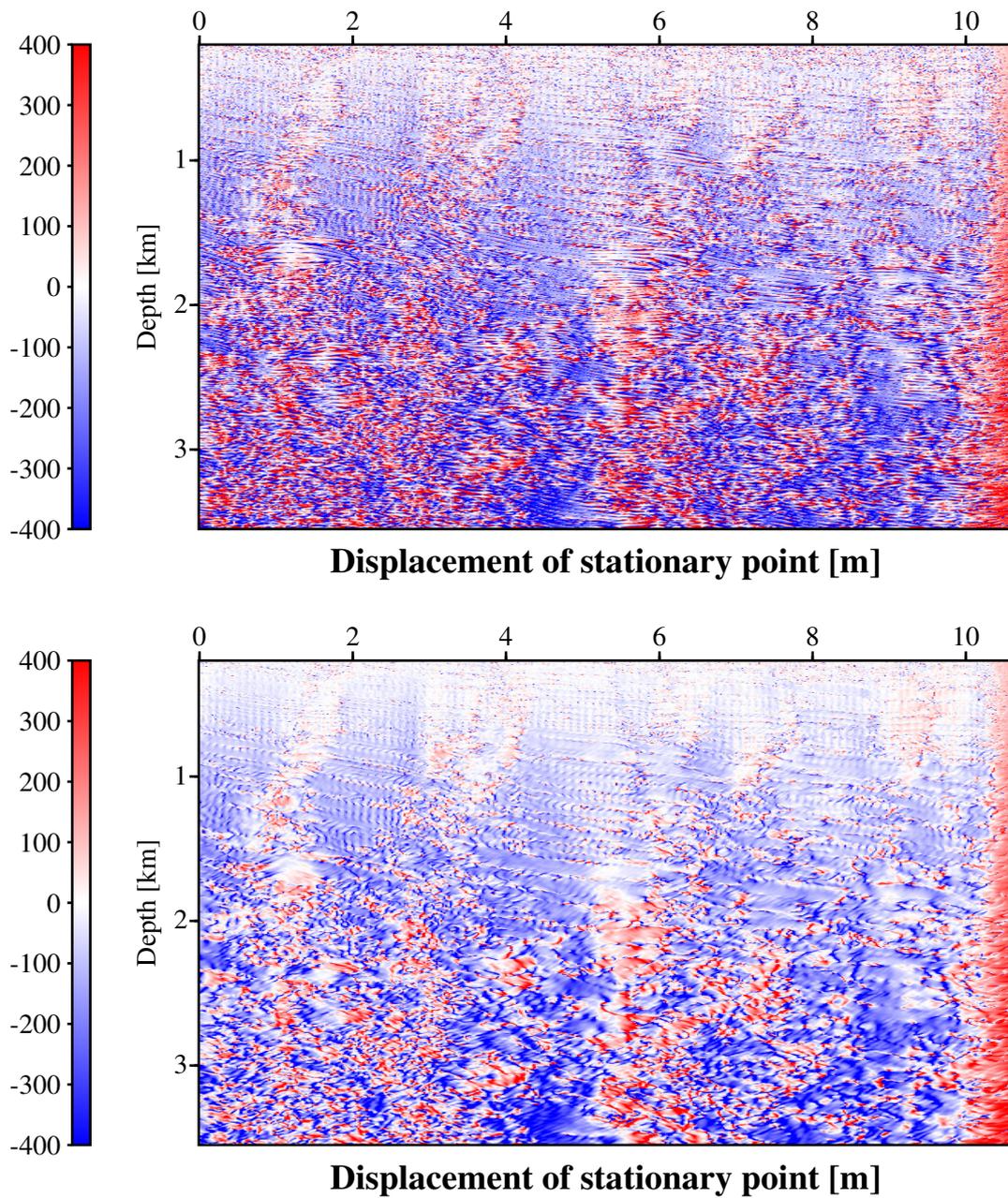


Figure 5: Real land data: top: displacement of stationary point with respect to the lateral image position. Bottom: the same displacement calculated from the envelopes of the migration results.

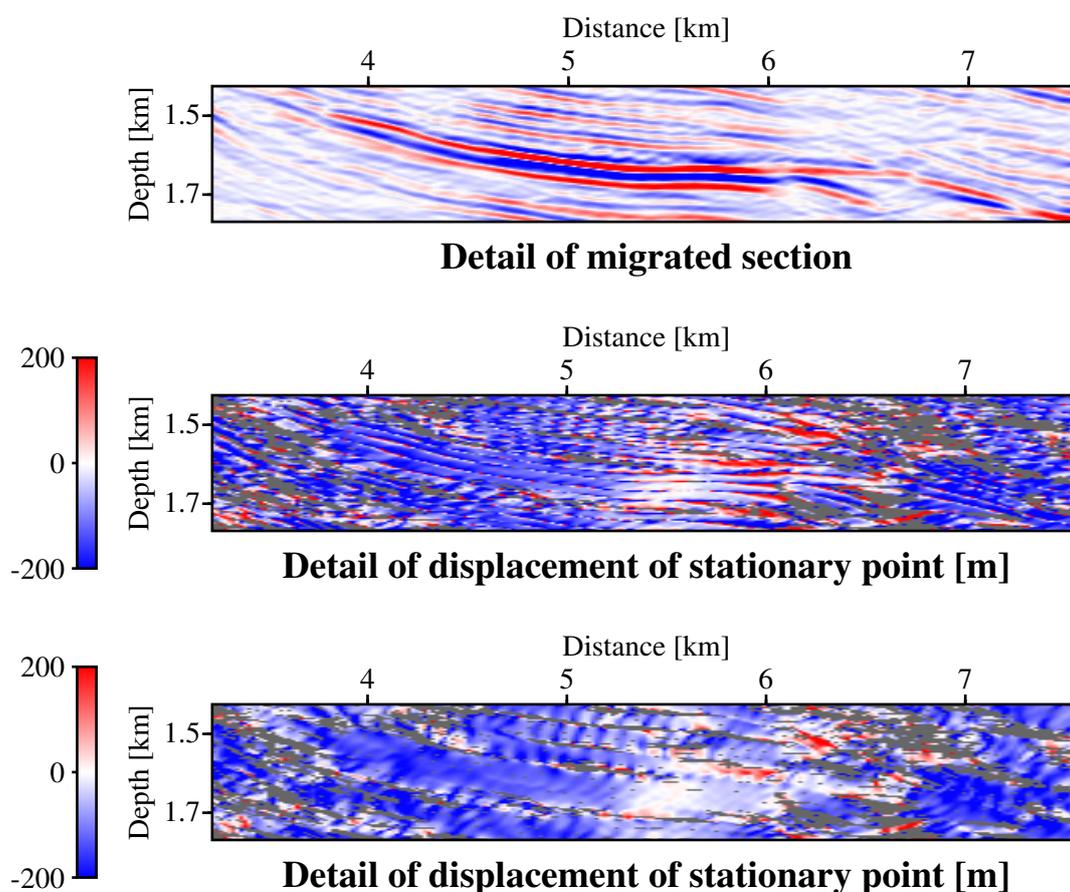


Figure 6: Real land data: top: detail of the migrated section shown in Figure 4. Middle: corresponding detail of displacement shown in Figure 5. Bottom: detail of displacement calculated from the envelopes of the migration results. Values not located on reflector images have been masked out.

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